

# Wilson Tank Replacement Colorado Springs, Colorado

July 27, 2021 (Revised November 18, 2021) Terracon Project No. 23215020

## **Prepared for:**

Kimley-Horn & Associates, Inc. Colorado Springs, Colorado

## Prepared by:

Terracon Consultants, Inc. Colorado Springs, Colorado

Environmental Facilities Geotechnical Materials



Kimley-Horn & Associates, Inc. 4582 South Ulster Street, Suite 1500 Colorado Springs, Colorado 80237

Attn: Mr. Adam Monchak

P: (720) 943-9961

E: Adam.Monchak@kimley-horn.com

Re: Geologic Hazards Study

Wilson Tank Replacement

6570 Alabaster Way

Colorado Springs, Colorado Terracon Project No. 23215020

Dear Mr. Monchak:

Terracon Consultants, Inc. (Terracon) has prepared a Geologic Hazard Study for the above referenced project. This study was performed in general accordance with Terracon Proposal No. P23215020 dated June 15, 2020. This report presents the findings on geologic hazards for the proposed project.

We appreciate the opportunity to be of service to you on this project. If you have any questions concerning this report or if we may be of further service, please contact us.

Sincerely,

Terracon Consultants, Inc.

Tyler A. Compton, P.E. Group Manager

3 down on

Scott B. Myers, P.E.

Senior Regional Consultant

Terracon Consultants, Inc. 4172 Center Park Drive Colorado Springs, Colorado 80916 P (719) 597 2116 F (719) 597 2117 terracon.com



APPLICATION FORM FOR GEOLOGIC HAZARD REPORT				
Applicant: Kimley-Horn	& Associates, Inc.	Telephone	719-453-0180	Fax
Address: 2 North Nevada Aver	nue, Suite 300, Colorado Springs, CO	Zip Code	80903	e-mail Adam.Monchak@kimley-horn.cor
Premises Involved: Develop	ment Plan/Subdivision Plat Name	: Wilson	Гank	
Tax Schedule No(s) 7 3	$\underline{1}$ $\underline{5}$ $\underline{2}$ - $\underline{0}$ $\underline{0}$ - $\underline{0}$ $\underline{0}$ are El Paso County Tax Assessor lo	3	_	the 2 <sup>nd</sup> Floor; phone: 520-6600
<u>GEOL</u> (	OGIC HAZARD REPORT REQ	OUIRED: (F	VE (5) PRELIMIN	ARY COPIES)
An application review fee wi The fee schedule is as follow	Il be required to accompany these s:	applications (	make checks payable	e to City of Colorado Springs).
Review of Geologic Hazard Reports			\$300 plus any Co	Planning Fee: Dolorado Geological Survey Cost Over \$300
			<u>City E</u>	ngineering Fee: \$284
Landscape Plan (if applicable	•	/ Horn, date	d November 5, 200	- 21 (Paviowad)
	Erosion Control Plan by Kimley	/-Horn date	d November 5, 202	- 21 (Reviewed)
	f debris and/or mud flow hazard is			_
Professiona	fied to prepare a Geolog of Colorado Springs.  al Geologist as defin	PS STATEM	ordance with the prov	visions of Section 504 of the
of the Colo	ority as defined by C. 107	St. me or Profe 7(1).	engineers and Pro	ng in Natural Hazard Areas" fessional Land Surveyors. November 18, 2021
This Geologic Hazard Study	~ 1	Sac of the C	<del></del>	olorado Springs, 2001, as amended.
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For the City Engineer	Date	City	Planning Director	Date

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Last Modified: 1/1/2010

## REPORT TOPICS

INTRODUCTION	1
SITE CONDITIONS	1
PROJECT DESCRIPTION	2
GEOTECHNICAL CHARACTERIZATION	3
POTENTIAL GEOLOGIC HAZARDS	5
GENERAL COMMENTS	10

**Note:** This report was originally delivered in a web-based format. **Orange Bold** text in the report indicates a referenced section heading. The PDF version also includes hyperlinks which direct the reader to that section and clicking on the **GeoReport** logo will bring you back to this page. For more interactive features, please view your project online at client.terracon.com.

## **ATTACHMENTS**

SITE LOCATION
SITE LOCATION WITH GEOLOGIC OVERLAY
SITE-SPECIFIC GEOLOGIC MAP
SITE LOCATION WITH LANDSLIDE OVERLAY
SITE LOCATION WITH DIPPING BEDROCK OVERLAY
EXPLORATION PLAN WITH AERIAL OVERLAY
EXPLORATION PLAN WITH DEVELOPMENT PLAN OVERLAY
EXPLORATION AND TESTING PROCEDURES
PHOTOGRAPHY LOG
EXPLORATION RESULTS
SUPPORTING INFORMATION

Note: Refer to each individual Attachment for a listing of contents.

#### **Geologic Hazards Study Report**

Wilson Tank Replacement ■ Colorado Springs, Colorado
July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020



## REPORT SUMMARY

A Geologic Hazards Study has been performed for the proposed Wilson Tank Replacement project to be located at 6570 Alabaster Way in Colorado Springs, Colorado. We offer the following comments regarding geologic hazards:

- Based on our review of the available geologic literature and experience in the project vicinity, potential geologic hazards have been identified at the site that may impact the proposed development. These include the potential to encounter localized man-made slope instability and steeply dipping bedrock within foundation bearing elevations.
- The site is considered suitable for the proposed development provided that the geologic hazards discussed herein are appropriately mitigated during the design and construction phases of the project.
- This report should be used in conjunction with the Geotechnical Engineering Report by Terracon issued under Project Number 23205020 revised October 29, 2021.

This summary should be used in conjunction with the entire report. It should be recognized that details were not included or fully developed in this section, and the report must be read in its entirety for a comprehensive understanding of the items contained herein. The section titled **GENERAL COMMENTS** should be read for an understanding of the report limitations.

## Wilson Tank Replacement 6570 Alabaster Way

## **Colorado Springs, Colorado**

Terracon Project No. 23215020 July 27, 2021 (Revised November 18, 2021)

## INTRODUCTION

This report presents the results of our Geologic Hazards Study performed for the proposed Wilson Tank Replacement project to be located at 6570 Alabaster Way in Colorado Springs, Colorado. The purpose of these services is to provide Geologic Hazards information in accordance with the City of Colorado Springs City Code relative to, but not limited to:

- Unstable or potentially unstable slopes
- Landslide or potential landslide areas
- Undocumented fill soils and landfills
- Ground subsidence and mining activity
- Debris flow and debris fans
- Rockfall
- Groundwater springs

- Expansive soils and expansive rock
  - Shallow water tables
- Flood prone areas
- Collapsible soils
- Steeply dipping bedrock
- Faults
- Radon

## SITE CONDITIONS

The following description of surficial site conditions is derived from our review of publicly available aerial and topographic maps.

Item	Description		
	The project is located at 6570 Alabaster Way in Colorado Springs, Colorado.		
Parcel Information	Approximate Latitude/Longitude: 38.9215° N, 104.8850° W		
	See Site Location		
Existing Improvements	The site is developed with a 164.5-foot diameter by 32.5-foot tall above ground, welded steel potable water storage tank. The total capacity of the tank is reported to be 5 million gallons.		
Current Ground Cover	Native grasses and weeds within the interior fenced area. An existing gravel-surfaced access road is also present at the site.		

Wilson Tank Replacement ■ Colorado Springs, Colorado
July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020



Item	Description		
Existing Topography	Topography at the proposed tank location is relatively flat based on a provided site layout. Existing slopes of approximately 2H:1V (Horizontal:Vertical) are located to the west and south of the proposed tank location. Slopes to the west of the proposed tank are up to approximately 14-feet in height and tapper to surrounding grades south of the proposed tank location.		

## **PROJECT DESCRIPTION**

Our final understanding of the project conditions is as follows:

Item	Description
Information Provided	<ul> <li>Request for Proposal RFP-LV-159074</li> <li>RFP-LV-159074 Addendum 1, dated March 17, 2021</li> <li>Geotechnical Checklist and Criteria, prepared by DN Tanks, dated April 18, 2014.</li> <li>90% Submittal Grading and Erosion Control Plan, dated November 5, 2021.</li> <li>Meeting with our client on August 24, 2021 and November 11, 2021</li> <li>Initial Review Letter – Development Plan and Final Subdivision Plat for CSU Wilson Tank Site dated September 8, 2021</li> </ul>
Project Description	We understand the existing tank was constructed in 1966 with an associated pump station. The tank was inspected in 2018 and it was determined that due to extensive corrosion, the existing tank will be replaced with a new concrete tank. The new tank will be constructed adjacent to the existing tank and will also be about 164.5 feet in diameter by 32.5 feet tall. We understand the new tank will either be a wire-wound pre-stressed concrete tank conforming to AWWA D110 Type III or a tendon prestressed concrete tank conforming to AWWA D115. The existing tank will remain in operation until the new tank is built.
Finished Floor Elevation	Reportedly 7101.45 feet
Grading/Slopes	Up to 5-feet of cut and 1-foot of fill is expected to be required to develop final grade in the proposed tank location.  Final constructed slopes of a maximum of 50 percent and up to about 15 feet in height are reported to the west, and tapering to existing grades to the south of the proposed new tank location. Existing slopes along the northwest side of the proposed new tank location with slopes of up to about 2H:1V are reported to remain.
Free-Standing Retaining Walls	None reported as part of site development.

Wilson Tank Replacement ■ Colorado Springs, Colorado
July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020



Item	Description
Below Grade Structures	Below grade structures are not planned as part of site development.
<b>Detention Pond</b>	Detention pond construction has not been reported for this site.

## **GEOTECHNICAL CHARACTERIZATION**

## **Regional Geology**

The proposed area is located within the Colorado Piedmont section of the Great Plains physiographic province. The Colorado Piedmont, formed during Late Tertiary and Early quaternary time (approximately two-million years ago), is a broad, erosional trench which separates the Southern Rocky Mountains from the High Plains. Structurally, the site lies along the western flank of the Denver Basin. During the Late Mesozoic and Early Cenozoic Periods (approximately seventy million years ago), intense tectonic activity occurred, causing the uplifting of the Front Range and associated downwarping of the Denver Basin to the east. Relatively flat uplands and broad valleys characterize the present-day topography of the Colorado Piedmont in this region.

## Site Specific Geology

Surficial geologic conditions at the site, as mapped by the Colorado Geological Survey (CGS) (<sup>1</sup>Morgan et al., 2003), consist of pediment gravel two.

Pediment gravel two has been described as medium-red to brown, poorly sorted, moderately to poorly stratified pebble, cobble, and boulder gravel primarily derived from granitic bedrock. Basal portion of unit contains layers of clay and silt interbedded with coarse-grained sand, cobble, and rare boulder gravels. Clasts are highly weathered and are coated with a thin (0.05 in.), discontinuous rind of calcium carbonate. Matrix typically consists of feldspar and quartz sand derived from weathered clasts. Becomes richer in boulders and less stratified toward mountain front. Top of pediment gravel is 130 to 215 ft above adjacent modern streams. The unit is considered to be middle Pleistocene on the basis of local stratigraphic and physiographic position and soil development.

Surficial observations from our site visit were used in combination with the subsurface information obtained from soil borings advanced at the site to develop a site-specific geologic map. The site-specific geologic map is included as an attachment to this report.

<sup>&</sup>lt;sup>1</sup>Morgan, M.L., Siddoway, C.S., Rowley, P.D., Temple, J., Keller, J.W., Archuleta, B.H., and Himmelreich, J.W., 2003, **Geologic Map of the Cascade Quadrangle, El Paso County, Colorado**, Colorado Geological Survey, Open-File Map 03-18, scale 1:24.000.

Wilson Tank Replacement ■ Colorado Springs, Colorado
July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020



The surficial site soils were underlain by sandstone and claystone bedrock, presumably of the Mesozoic and Paleozoic Rock Unit, starting at depths of about 3½ to great than 42 feet below existing site grades.

## **Typical Profile**

Based on our field investigation, subsurface conditions consist of the following:

Description	Approximate Depth to Bottom of Stratum <sup>2</sup>	Material Encountered	Density/Stiffness/ Hardness
Stratum 1	3½ to 42 feet <sup>1</sup>	Sand with varying amounts of clay, silt, and gravel	Medium dense to very dense
Stratum 2	49½ feet <sup>1</sup>	Sandstone and claystone bedrock	Very hard

- 1. Includes total depths explored where borings were terminated in a stratum and the total depth is unknown.
- 2. Below existing ground surface.

#### **Groundwater Conditions**

The boreholes were observed while drilling and sampling for the presence and level of groundwater. Boring B-103 was left open for approximately 24 hours after drilling and sampling, and the boring was observed for the presence of groundwater again at that time. Groundwater was not observed in the borings completed at the site.

Groundwater level fluctuations occur due to seasonal variations in the amount of rainfall, runoff and other factors not evident at the time the borings were performed. Therefore, groundwater levels during construction or at other times in the life of the structure may be higher or lower than the levels indicated on the boring logs. The possibility of groundwater level fluctuations should be considered when developing the design and construction plans for the project.

Zones of perched and/or trapped groundwater may also occur at times in the subsurface soils overlying bedrock, on top of the bedrock surface or within permeable fractures in the bedrock materials. The location and amount of perched water is dependent upon several factors, including hydrologic conditions, type of site development, irrigation demands on or adjacent to the site, seasonal fluctuations, and weather conditions.

## **Laboratory Testing**

Laboratory test results indicate that the sand soils tested exhibit low compression when subjected to an applied load of 500 pounds per square foot (psf) at in-situ water contents. When exposed

Wilson Tank Replacement ■ Colorado Springs, Colorado
July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020



to increases in moisture content at an applied load of 500 psf, the sand soils tested exhibit negligible to low compression followed by low to very high compression at increased loadings. It is our opinion that the sample of sand soils tested was disturbed either during sampling or sample preparation and the observed moderate to very high compression is not representative of the insitu conditions of the on-site sand soils. Based on our experience, the on-site sand soils would be considered to exhibit low to moderate compression when subjected to increased moisture and loading conditions.

The results of laboratory testing completed for this project can be found in the **Exploration Results** section of this report.

## POTENTIAL GEOLOGIC HAZARDS

Our study considered the following potential geologic hazards and their risk to impact the project site.

## **Unstable or Potentially Unstable Slopes and Landslide Areas**

Surficial geologic conditions at the site, as mapped by the Colorado Geological Survey (CGS) (<sup>2</sup>White and Wait), indicates that evidence of landslide susceptibility has not been observed at the site. Slopes associated with the drainage area of Douglas Creek located approximately 350 feet northwest of the proposed tank are mapped as a landslide susceptible area. Based on the distance from the proposed tank, the relatively shallow bedrock encountered at the site, and the identified landslide susceptible area slopping away from the site, it is our opinion the risk potential for landslide areas to impact the development is low.

The location of the proposed tank appears to have previously been graded by the removal of native soils to create a relatively level area for tank construction based on the topography of the adjacent slopes and surrounding grades. The existing slopes to the west and south of the proposed tank are reported to be on the order of 2H:1V based on the provided grading plan. Apparent signs of instability of the existing slopes in the form of scarps, surficial cracking, and/or surficial instability was not observed.

We understand the planned construction consists of cutting back the existing slopes a lateral distance of about 10 to 15 feet, and final slopes will be a maximum of 50 percent. Terracon performed a global slope stability analyses, attached, at a cross section where the proposed slope is about 50 percent and about 15 feet in height. Our analyses showed that the long-term global

<sup>&</sup>lt;sup>2</sup>White, J.L., and Wait, T.C., 2003, **Potential Areas of Landslide Susceptibility in Colorado Springs, El Paso County, Colorado**. Colorado Geological Survey, Map Series 42, Plate 1 of 3, scale 1:24,000.

Wilson Tank Replacement ■ Colorado Springs, Colorado
July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020



stability of the slope is sufficient for the subsurface conditions encountered and proposed slope geometry.

## Landfill, Uncontrolled, or Undocumented Fill Activity

Artificial fill soils were not encountered in our borings performed at the site. Indications of landfills (refuse and debris) were not observed in the samples collected during our field exploration.

Regrading of the site appears to have been previously performed to create a level area for the proposed tank based on the existing slope topography and surrounding grades, however it appears site grading consisted of removal of onsite soils (cut) and fill soils do not appear to have been placed based on our visual observation of the site and the information obtained from our borings. It is our opinion that the risk for artificial fill soils or landfills to impact the proposed development is low. Should artificial fill soils be encountered at the time of construction, it is our opinion that they can be remediated through conventional earthwork methods, such as removal and replacement as compacted, structural fill.

## **Underground Mining and Ground Subsidence**

The site is not located in an area previously mapped in the Colorado Geologic Survey Subsidence Investigation Report (<sup>3</sup>Dames and Moore, Inc., 1985). Based on this information, it is our opinion the risk potential for underground mining and ground subsidence to impact the development is low.

#### **Debris Flow and Debris Fan**

The site is not located in an area mapped with conditions favorable for the generation and deposition of debris flows ( $^4$ McCoy, Morgan, & Berry, 2018). Land upslope from the project site generally consists of native grasses and extends northwest approximately 350 feet up an approximately 12H:1V slope to drainage associated with Douglas Creek, and that drainage slopes away from the project site. Based on this information, it is our opinion that the potential for debris flows at the project site is considered low.

#### Rockfall

Evidence of rockfall was not observed on or within the immediate vicinity of the project site during our site visits. Exposed rock outcrops were not observed on the surface of the project site,

<sup>&</sup>lt;sup>3</sup> Dames & Moore, Inc., **1985, Colorado Springs Subsidence Investigation for Colorado Springs**, Volume IV: Maps, State of Colorado, Division of Mined Land Reclamation

<sup>&</sup>lt;sup>4</sup>McCoy, K.M., Morgan, M.L., & Berry, K.A., 2018, **Debris Flow Susceptibility Map of El Paso County, Colorado**, Colorado Geological Survey, Open-File Report 18-11, scale 1:24,000.

Wilson Tank Replacement ■ Colorado Springs, Colorado
July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020



overhanging the project site, or located in areas that have the potential for rockfall, therefore, it is our opinion there is a low potential for rockfall to occur on the site.

## **Shallow Water Tables and Groundwater Springs**

Based upon review of U.S. Geological Survey maps (<sup>5</sup>Hillier and Hutchinson, 1980), regional groundwater is expected to be encountered in alluvial deposits that are not perennially saturated, generally the groundwater table changes seasonally from depths of about 5 to 20 feet below present ground surface.

As noted in the **Geotechnical Characterization** section of this report, groundwater was not encountered in our borings completed at the site at the time of drilling, or when checked approximately 24 hours after drilling in Boring No. B-103. It is our opinion that there is a low risk of shallow groundwater impacting the development. It has been our experience that zones of perched and/or trapped groundwater may occur at times in the subsurface soils overlying bedrock, on top of the bedrock surface or within permeable fractures in the bedrock materials. The location and amount of perched water is dependent upon several factors, including hydrologic conditions, type of site development, irrigation demands on or adjacent to the site, seasonal fluctuations, and weather conditions. If encountered during construction, zones of perched and/or trapped groundwater will likely require case specific mitigation. If encountered, it is our opinion water can be mitigated during construction using conventional dewatering techniques, such as shallow trenches directing water away from the development, and the risk for groundwater to impact the proposed development is considered to be low.

#### Flood Prone Areas

Based on a review of the Federal Emergency Management Agency (FEMA) flood map 08041C0492G effective on December 7, 2018, the project site is located in Zone X, an area outside the 0.2% annual chance floodplain. It is our opinion that the risk of flooding on the project site is low.

## **Expansive Soils and Bedrock**

Mapping completed by the Colorado Geological Survey (<sup>6</sup>Hart, 1973-1974), indicates the site is in areas associated with low swell potential. Based on mapping, our laboratory testing, and our experience in the vicinity of the project site, it is our opinion that the encountered sand soils and

<sup>&</sup>lt;sup>5</sup>Hillier, D.E., and Hutchinson, E.C., 1980, **Depth to Water Table in the Colorado Springs – Castle Rock Area, Front Range Urban Corridor, Colorado**, United States Geological Survey, Miscellaneous Investigation Series Map I-857-H, scale 1:100,000

<sup>&</sup>lt;sup>6</sup>Hart, S.S., 1973-1974, **Potentially Swelling Soil and Rock in the Front Range Urban Corridor, Colorado**, Colorado Geological Survey, Sheet 3 of 4, scale 1:100,000.

Wilson Tank Replacement ■ Colorado Springs, Colorado

July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020



sandstone bedrock should be considered to have negligible to low expansive potential. Claystone bedrock was encountered in one boring completed at the site at a depth of approximate 37 feet and should be considered to have low to high expansive potential. However, the potential exists for claystone bedrock to exist at other locations and at shallower depths at the site. Because steeply dipping bedrock may exist on this site, there may be areas of shallow claystone bedrock exposed during construction. To account for this possibility and the potential effects of expansive claystone bedrock, we have recommended in our Geotechnical Engineering Report that a minimum 10-foot separation be maintained between the top of bedrock and the bottom of foundations.

Based on the information listed above, and provided the recommendations listed above and in our Geotechnical Engineering Report are followed in the design and construction of the proposed tank, it is our opinion that the risk of expansive potential associated with the claystone bedrock to impact the proposed development is low.

## **Collapsible Soils**

Mapping completed by the U.S. Geological Survey (<sup>7</sup>Madole) indicates the site is not located in an area that contains eolian sand deposits known to have collapse potential. Negligible to low collapse was observed in the soil samples tested when inundated with water. Based on the results of our field exploration and laboratory testing, the risk of collapsible soils to impact the development is considered low. Compressible soils, if observed at the time of construction, can be mitigated using remedial grading activities.

#### **Steeply Dipping Bedrock**

The site is mapped approximately 150 feet west of an area mapped (8Himmelreich Jr, and Noe, 1999) as susceptible to differential heave in expansive, steeply dipping bedrock. Our borings completed within the proposed tank footprint encountered bedrock at depths ranging from approximately 3½ feet to 37 feet below existing grade, and bedrock was not encountered in Boring No. B-104 (termination depth of 40½ feet). Additionally, rock outcroppings located approximately 1/4 mile southwest of the site appear to possess near-vertical dip direction based on our visual observations from the site. Although not observed in the bedrock samples obtained from our borings, it is our opinion that dipping bedrock is likely present at this site and we recommend the follow mitigation procedures for the proposed development.

<sup>&</sup>lt;sup>7</sup>Madole, R.F., VanSistine, D.P., Michael, J.A., 2005, **Distribution of Late Quaternary Wind-Deposited Sand in Eastern Colorado**, United States Geological Survey, Scientific Investigations Map 2875, scale 1:700,000.

<sup>&</sup>lt;sup>8</sup>Himmelreich Jr., J.W., Noe, D.C., 1999, **Map of Areas Susceptible to Differential Heave in Expansive, Steeply Dipping Bedrock, City of Colorado Springs, Colorado**, Colorado Geological Survey, Map Series 32, scale 1:24,000.

Wilson Tank Replacement ■ Colorado Springs, Colorado
July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020



- The proposed tank should not be constructed on deep foundations supported on bedrock.
- The proposed tank should be constructed on shallow foundations supported on a minimum 10-foot thick zone of structural fill, such that a minimum 10-foot separation exists between the lowest foundation element and the top of bedrock. This is anticipated to require excavation of existing bedrock within portions of the tank footprint.

Provided the recommendations listed above and in our Geotechnical Engineering Report are followed in the design and construction of the proposed tank, it is our opinion that the risk of differential heave associated with steeply dipping bedrock is low.

## Hillside and Streamside Overlay

The site is within the hillside overlay according to the City of Colorado Springs, Hillside Overlay Map, dated August 2008, and will be subject to the applicable reviews and permits. The site is not located within the streamside overlay according to the City of Colorado Springs, Streamside Overlay Map, dated March 2009.

#### Radon

We are not aware of any basements or low-lying areas being incorporated into the design of the development. Additionally, the proposed structure will be uninhabited. Radon is often found in basements, crawl spaces, or other low-lying, poorly ventilated areas. The risk for lowest floor radon collection to impact the development is likely low.

## **Shallow Bedrock**

Very hard bedrock was encountered on the project site at depths of about 3½ to greater than 40½ feet (maximum exploration depth in Boring B-104) below existing ground surface. Shallow foundations placed on structural fill to support the new developments are expected to encounter bedrock within portions of the site. For excavations that will encounter bedrock, specialized equipment and/or techniques may be required. It is our opinion that equipment and techniques exist to extend excavations into bedrock, and the risk of shallow bedrock to cause differential foundation movement is considered low provided the recommendations contained herein and in our Geotechnical Engineering Report are followed during construction. We recommend the owner solicit bedrock excavations requests from local excavation contractors to provide recommended equipment, means, and methods to properly excavate bedrock at this site.

## **Erosion**

The surficial soils are likely susceptible to wind and water erosion. It is our opinion that the risk of erosion impacting the site is low if disturbed areas are re-vegetated after construction, and slopes are faced with erosion protection such as concrete or grouted rip-rap. However, additional regrading and maintenance may be required if erosion begins to affect site grades after

Wilson Tank Replacement ■ Colorado Springs, Colorado
July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020



construction. Water or other methods may be needed for dust suppression during construction. We recommend a maintenance plan be developed and followed to observe completed slopes after development and make appropriate as needed repairs due to erosion. Further, because the site is located within the hillside overlay area we understand a Grading and Erosion Control Plan will be required.

#### **Faults**

The closest fault is the Rampart Range Fault, located approximately 0.35 miles west of the project site, and a series of associated, inferred faults that traverse the project area. The Rampart Range Fault is a Quaternary age fault with a normal sense of movement and no assumed movement in the past 30 to 50 ka (<sup>9</sup>Dickson). Colorado has previously been mapped as an area with very low seismic risk and is currently rated to have low to moderate earthquake hazard. Based on the low seismicity in the project area, it is our opinion that the risk of earthquakes affecting the development is low.

## **GENERAL COMMENTS**

Our analysis and opinions are based upon our understanding of the project, the geotechnical conditions in the area, and the data obtained from our site exploration. Natural variations will occur between exploration point locations or due to the modifying effects of construction or weather. The nature and extent of such variations may not become evident until during or after construction. Terracon should be retained as the Geotechnical Engineer, where noted in this report, to provide observation and testing services during pertinent construction phases. If variations appear, we can provide further evaluation and supplemental recommendations. If variations are noted in the absence of our observation and testing services on-site, we should be immediately notified so that we can provide evaluation and supplemental recommendations.

Our Scope of Services does not include either specifically or by implication any environmental or biological (e.g., mold, fungi, bacteria) assessment of the site or identification or prevention of pollutants, hazardous materials or conditions. If the owner is concerned about the potential for such contamination or pollution, other studies should be undertaken.

Our services and any correspondence or collaboration are intended for the sole benefit and exclusive use of our client for specific application to the project discussed and are accomplished in accordance with generally accepted geotechnical engineering practices with no third-party beneficiaries intended. Any third-party access to services or correspondence is solely for

<sup>&</sup>lt;sup>9</sup>Dickson, P.A., 1986, Investigation of the Rampart Range fault at the Air Force Academy trench site, Colorado Springs, Colorado, in Rogers, W.P., and Kirkham, R.M., eds., Contributions to the Colorado tectonics and seismicity – A 1986 update: Colorado Geological Survey Special Publication 28, p. 172-185

Wilson Tank Replacement ■ Colorado Springs, Colorado
July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020



information purposes to support the services provided by Terracon to our client. Reliance upon the services and any work product is limited to our client, and is not intended for third parties. Any use or reliance of the provided information by third parties is done solely at their own risk. No warranties, either express or implied, are intended or made.

Site characteristics as provided are for design purposes and not to estimate excavation cost. Any use of our report in that regard is done at the sole risk of the excavating cost estimator as there may be variations on the site that are not apparent in the data that could significantly impact excavation cost. Any parties charged with estimating excavation costs should seek their own site characterization for specific purposes to obtain the specific level of detail necessary for costing. Site safety, and cost estimating including, excavation support, and dewatering requirements/design are the responsibility of others. If changes in the nature, design, or location of the project are planned, our conclusions and recommendations shall not be considered valid unless we review the changes and either verify or modify our conclusions in writing.

## **ATTACHMENTS**

## **Contents:**

Site Location
Site Location with Geology Overlay
Site-Specific Geologic Map
Site Location with Potential Areas of Landslide Susceptibility
Site Location with Dipping Bedrock Overlay
Exploration Plan with Aerial Overlay
Exploration Plan with Development Plan Overlay
Exploration and Testing Precedures

Exploration and Testing Procedures

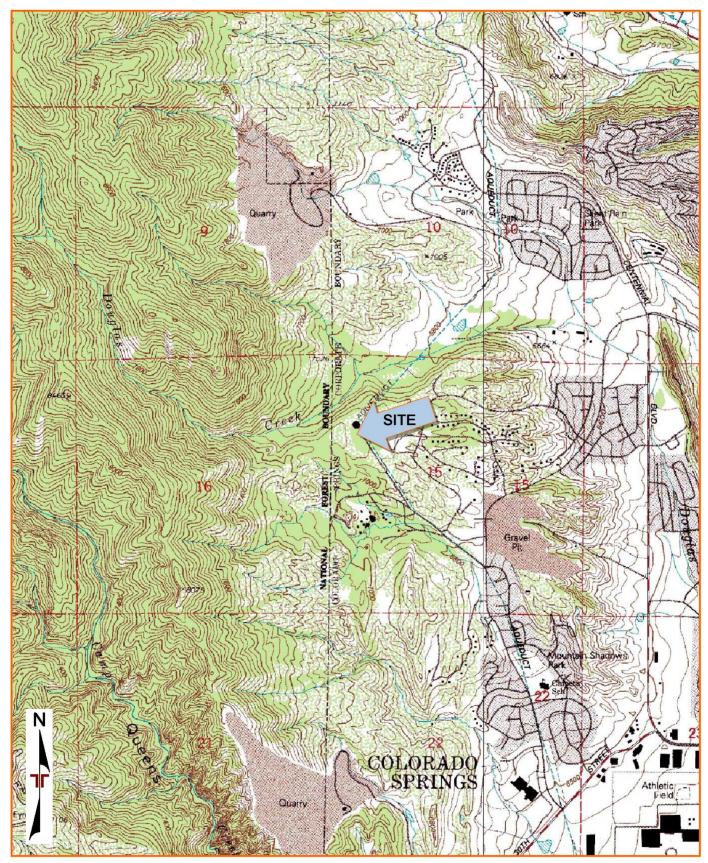
Photography Log Exploration Results

**Supporting Information** 

Note: All attachments are one page unless noted above.

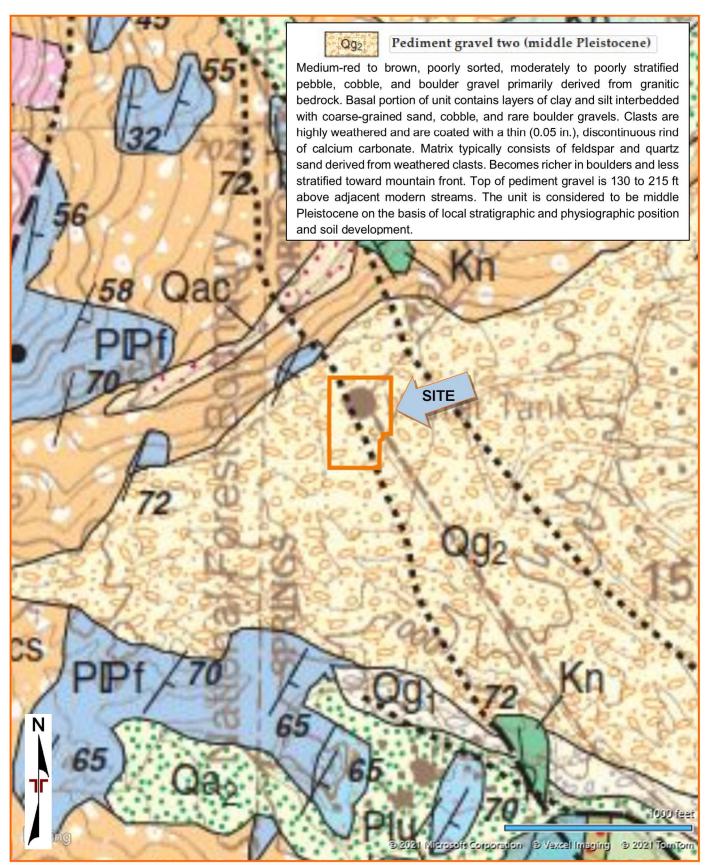
## SITE LOCATION





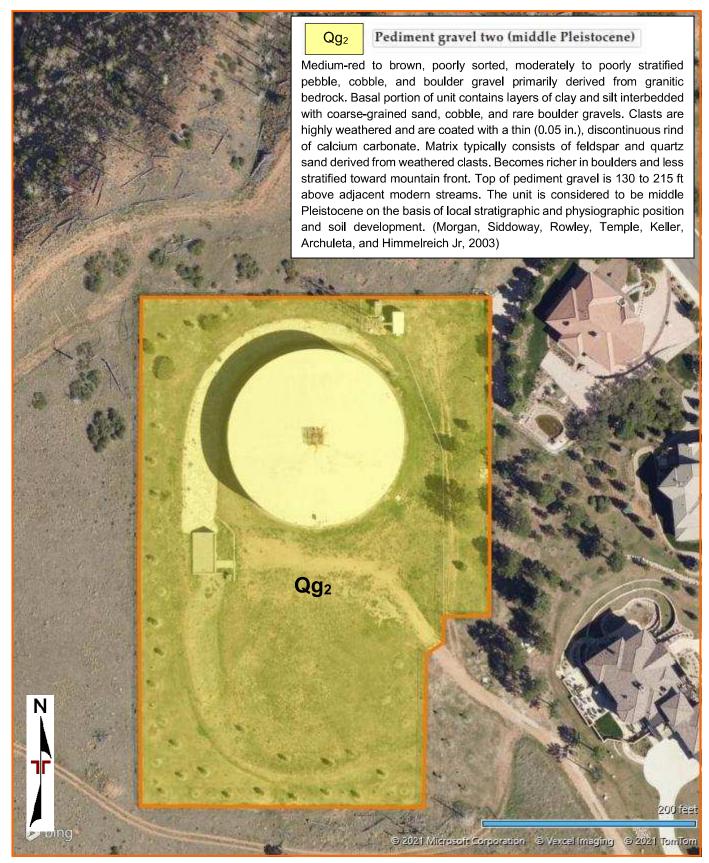
#### SITE LOCATION WITH GEOLOGIC OVERLAY





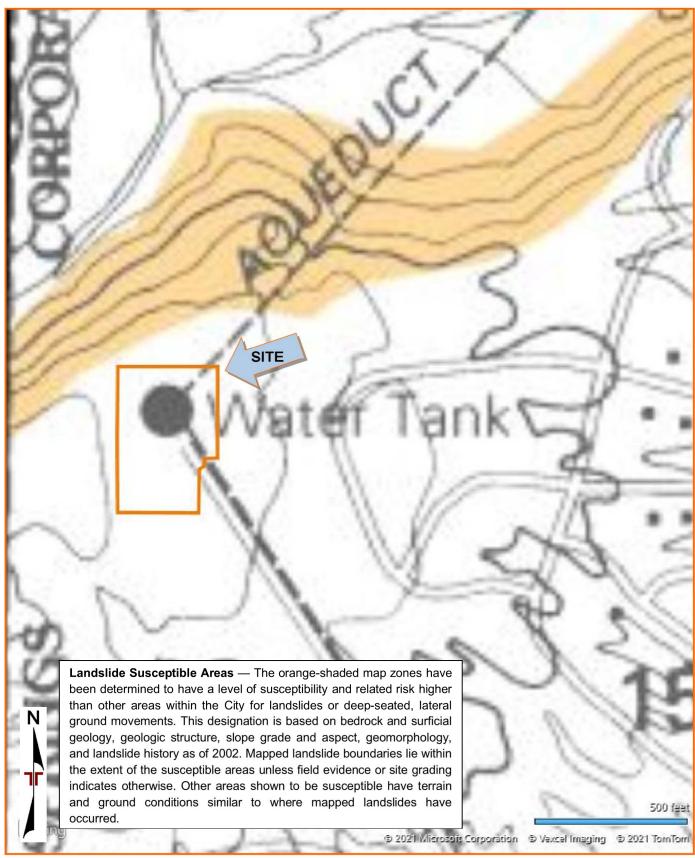
#### SITE-SPECIFIC GEOLOGIC MAP





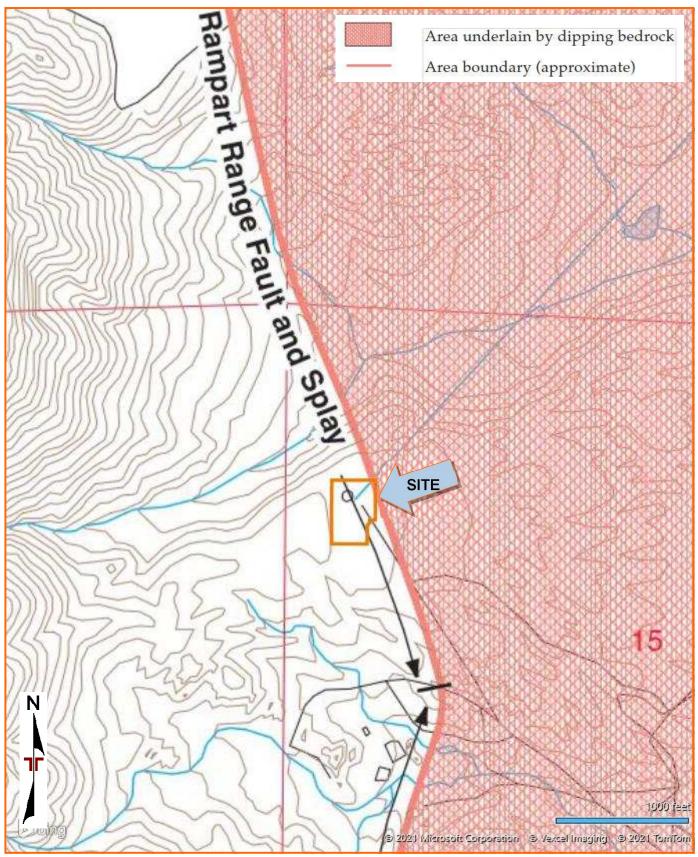
#### SITE LOCATION WITH LANDSLIDE OVERLAY





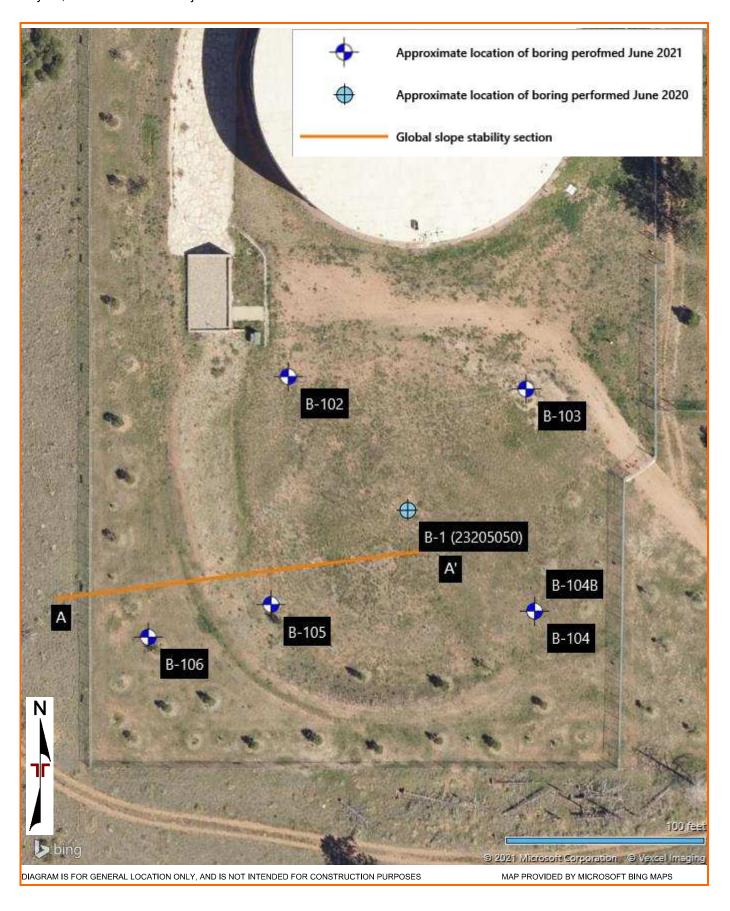
#### SITE LOCATION WITH DIPPING BEDROCK OVERLAY





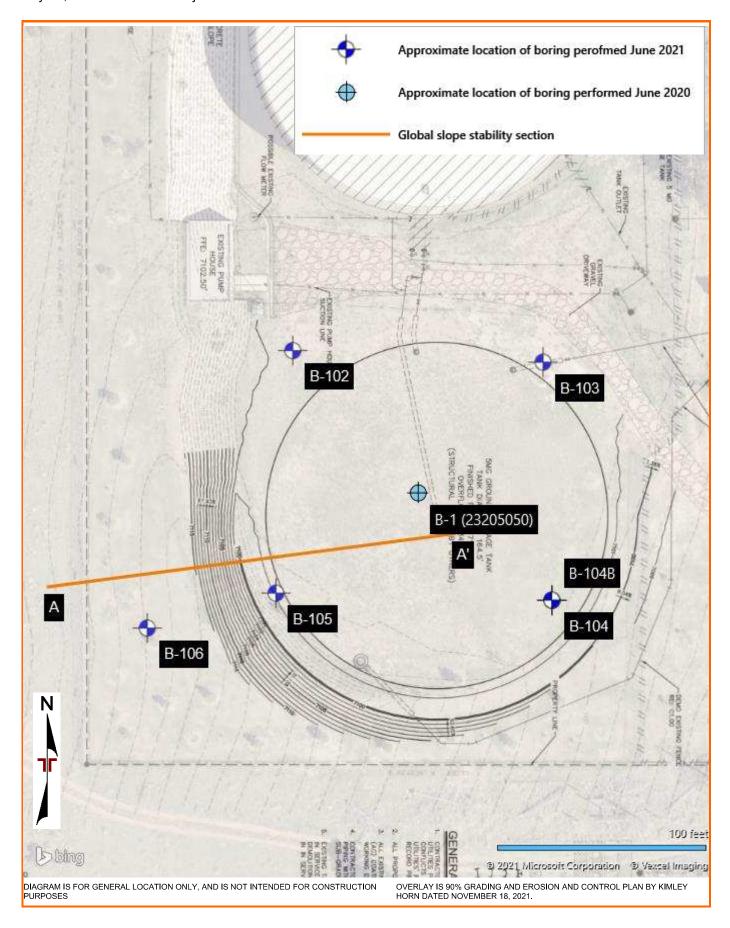
## **EXPLORATION PLAN WITH AERIAL OVERLAY**





## **EXPLORATION PLAN WITH SITE PLAN OVERLAY**







## **EXPLORATION AND TESTING PROCEDURES**

## **Field Exploration**

Number of Borings	Boring Depth (feet)	Location	
6	31 to 49.5	Planned tank area	
	31 10 49.5	(B-1, B-102 to B-106)	

**Boring Layout and Elevations:** We used handheld GPS equipment to locate borings with an estimated horizontal accuracy of ±20 feet. Approximate elevations were obtained by interpolation from the 60% Site and Grading Plan dated September 21, 2021, provided by Kimley-Horn.

**Subsurface Exploration Procedures:** We advanced the soil borings with a truck-mounted drill rig using continuous flight augers. Four samples were obtained in the upper 10 feet of each boring and at intervals of 5 feet thereafter. In the split-barrel sampling procedure, a standard 2-inch outer diameter split-barrel sampling spoon was driven into the ground by a 140-pound automatic hammer falling a distance of 30 inches. The number of blows required to advance the sampling spoon the last 12 inches of a normal 18-inch penetration was recorded as the Standard Penetration Test (SPT) resistance value. The SPT resistance values, also referred to as N-values, are indicated on the boring logs at the test depths. A 3-inch outer diameter split-barrel sampling spoon with 2.5-inch inner diameter ring lined sampler was used for sampling in the upper 14 to 19 feet. Ring-lined, split-barrel sampling procedures were similar to standard split spoon sampling procedure; however, blow counts were recorded for 6-inch intervals for a total of 12 inches of penetration. The samples were placed in appropriate containers, taken to our soil laboratory for testing, and classified by a geotechnical engineer. We did not encounter groundwater in our borings during drilling and sampling or when checked approximately 24 hours after drilling in Boring No. B. For safety purposes, all borings were backfilled with auger cuttings after their completion.

Our exploration team prepared field boring logs as part of standard drilling operations which included the sampling depths, penetration distances, and other relevant sampling information. Field logs include visual classifications of materials encountered during drilling, and our interpretation of subsurface conditions between samples. Final boring logs, prepared from field logs, represent the geotechnical engineer's interpretation, and include modifications based on observations and laboratory tests.

## **Laboratory Testing**

The project engineer reviewed the field data and assigned laboratory tests to understand the engineering properties of the various soil and rock strata, as necessary, for this project. The following testing was performed:

Wilson Tank Replacement ■ Colorado Springs, Colorado
July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020

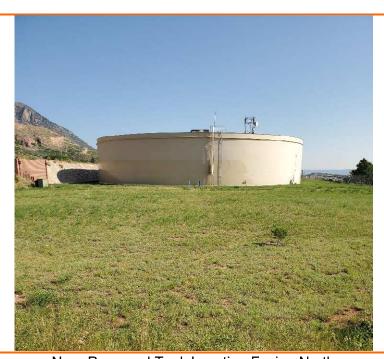


- Water content
- Unit dry weight
- Atterberg limits
- Grain size analyses
- Consolidation/expansion
- Chemical Analyses pH, Sulfates, Chloride Ion, Electrical Resistivity

The laboratory testing program included examination of the soil samples by an engineer. Based on the material's texture and plasticity, we described and classified the soil samples in accordance with the Unified Soil Classification System. Rock classification was performed using locally accepted procedures.



## **PHOTOGRAPHY LOG**



Near Proposed Tank Location Facing North



Near Proposed Tank Location Facing West

# Wilson Tank Replacement ■ Colorado Springs, Colorado July 27, 2021 (Revised November 18, 2021) ■ Terracon Project No. 23215020





Near Proposed Tank Location Facing South



Near Proposed Tank Location Facing East

## **EXPLORATION RESULTS**

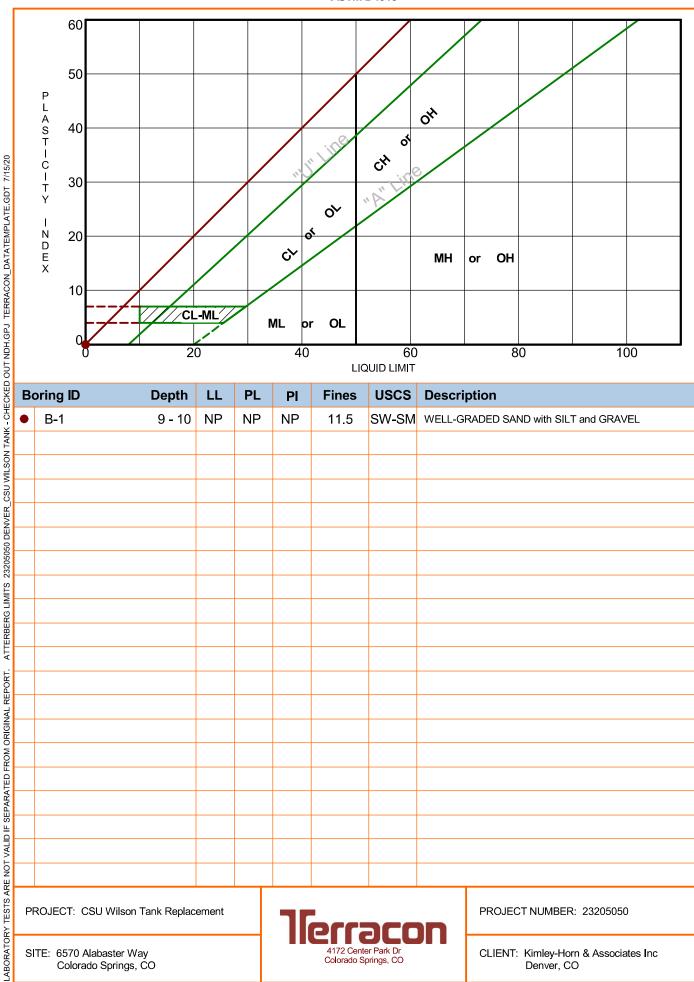
## **Contents:**

Boring Logs (B-1 (23205050), B-102 through B-105, B-104B, and B-106) Atterberg Limits (2 pages) Grain Size Distribution (2 pages) Consolidation/Swell (3 pages) Corrosivity (2 pages)

Note: All attachments are one page unless noted above.

### ATTERBERG LIMITS RESULTS

**ASTM D4318** 



	Вс	oring ID	Depth	LL	PL	PI	Fines	uscs	Description
5	•	B-1	9 - 10	NP	NP	NP	11.5	SW-SM	WELL-GRADED SAND with SILT and GRAVEL
F200									
2000									
ATTERBERG LIMITS 23203030 DENVER_CSO WILSON TAIN - CHECKEL									
2000									
0 7									
<u>≅</u> 9									
ζ									
ָ בְּ									
ר קר									
2									
Ō -									
7									
ARA									
RE NOT VALID IF SEPARATED FROM ORIGINAL REPORT.									
2									
뷛									

PROJECT: CSU Wilson Tank Replacement

SITE: 6570 Alabaster Way Colorado Springs, CO

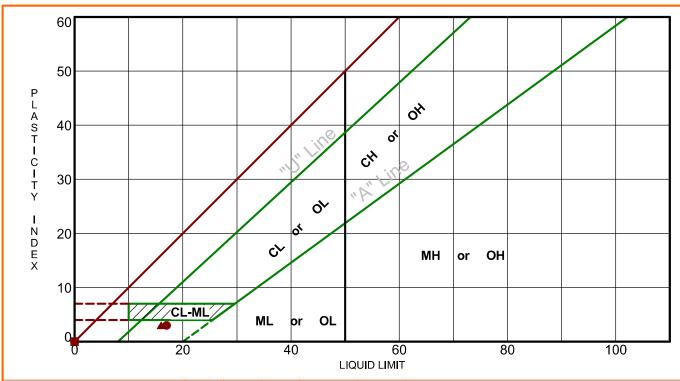


PROJECT NUMBER: 23205050

CLIENT: Kimley-Horn & Associates Inc Denver, CO

### ATTERBERG LIMITS RESULTS

**ASTM D4318** 



i,	Boring ID Depth		LL	PL	PI	Fines	USCS	Description			
•	B-103	9 - 10	17	14	3	24.3	SM	SILTY SAND			
	B-103	14 - 15	NP	NP	NP	14.5	SM	SILTY SAND with GRAVEL			
	B-103	19 - 20	16	13	3	26.8	SM	SILTY SAND			
ŀ	<b>▶</b> B-104	19 - 20	NP	NP	NP	3.3	SW	WELL-GRADED SAND with GRAVEL			
	B-105	9 - 10	NP	NP	NP	3.1	SW	WELL-GRADED SAND with GRAVEL			
•	B-106	9 - 10	NP	NP	NP	7.6	SW-SM	WELL-GRADED SAND with SILT and GRAVEL			
í o											
)											
i P											
5											
2											

PROJECT: Wilson Tank Replacement

SITE: 6570 Alabaster Way Colorado Springs, Colorado

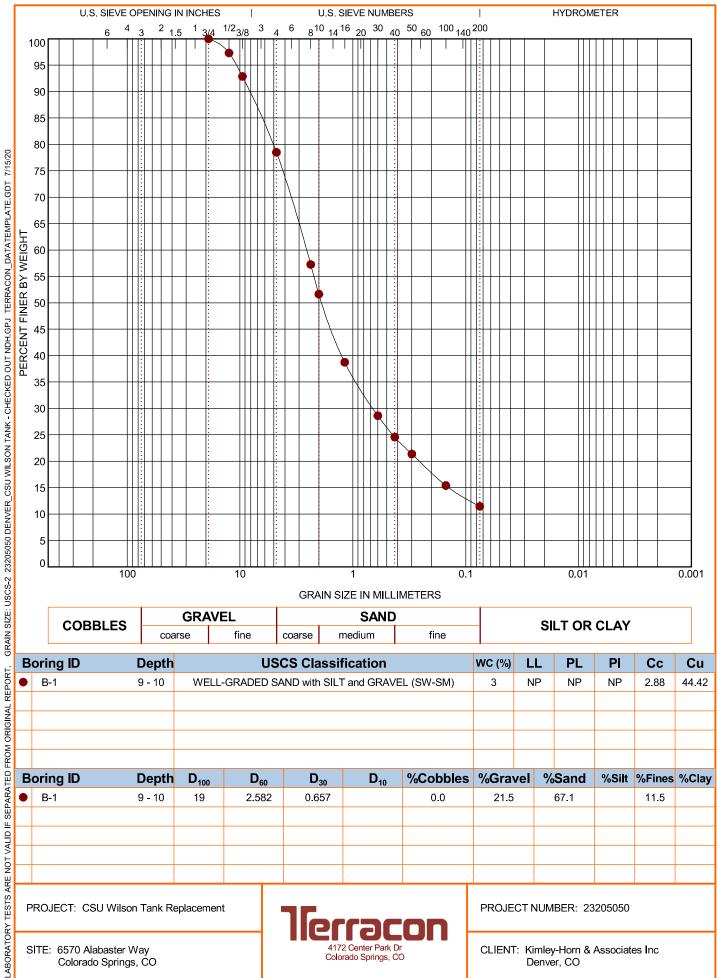


PROJECT NUMBER: 23215020

CLIENT: Kimley-Horn and Associates Inc Denver, Colorado

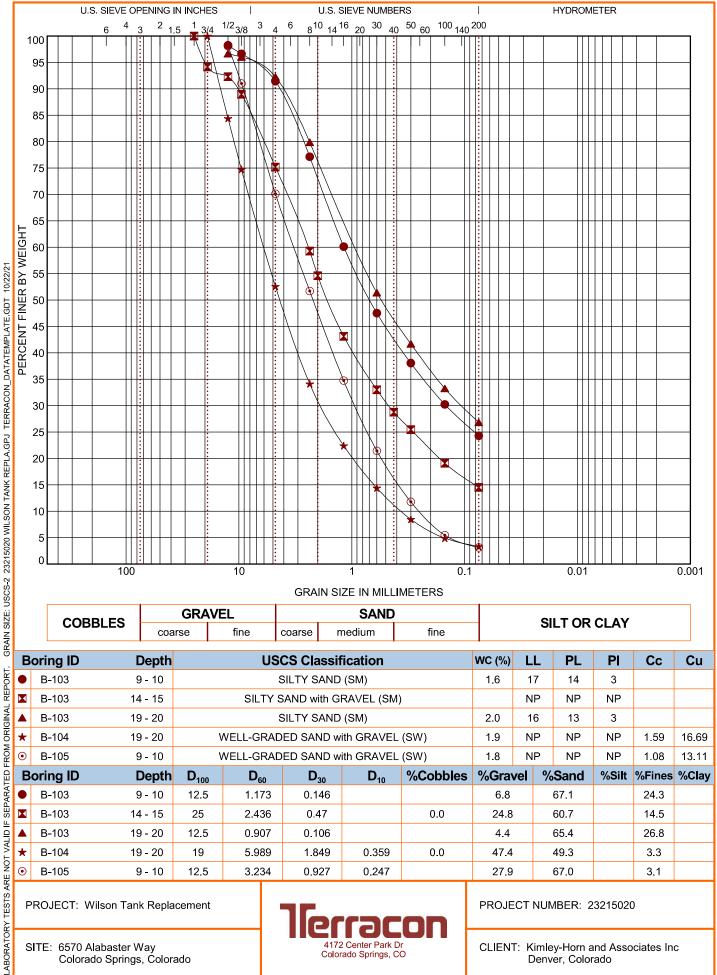
### **GRAIN SIZE DISTRIBUTION**

**ASTM D422 / ASTM C136** 



### GRAIN SIZE DISTRIBUTION

#### **ASTM D422 / ASTM C136**



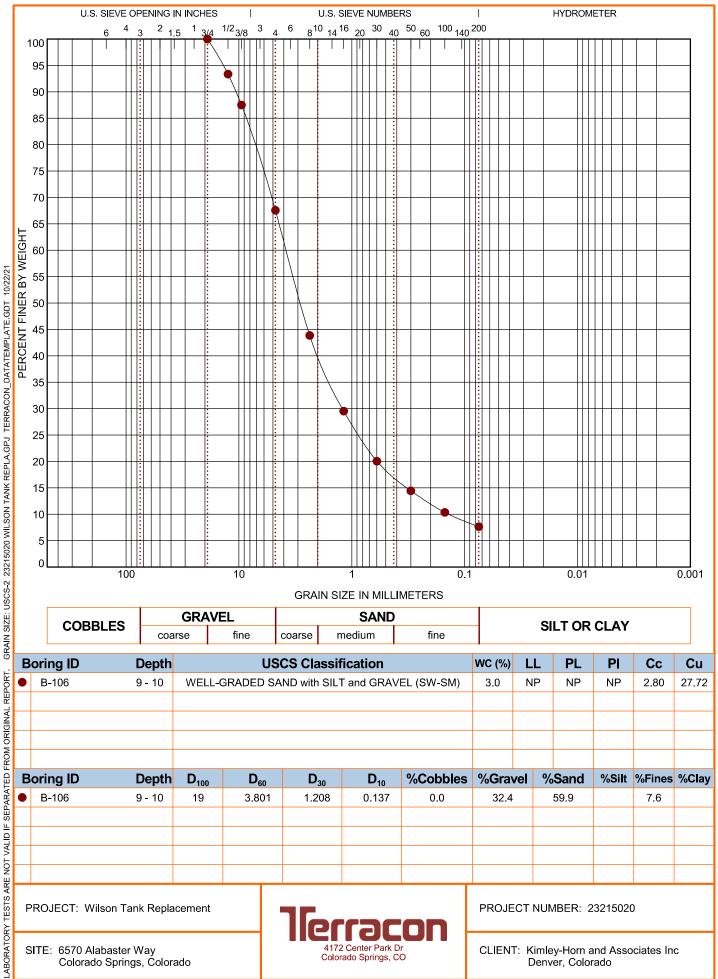
SITE: 6570 Alabaster Way Colorado Springs, Colorado Colorado Springs, CO

CLIENT: Kimley-Horn and Associates Inc

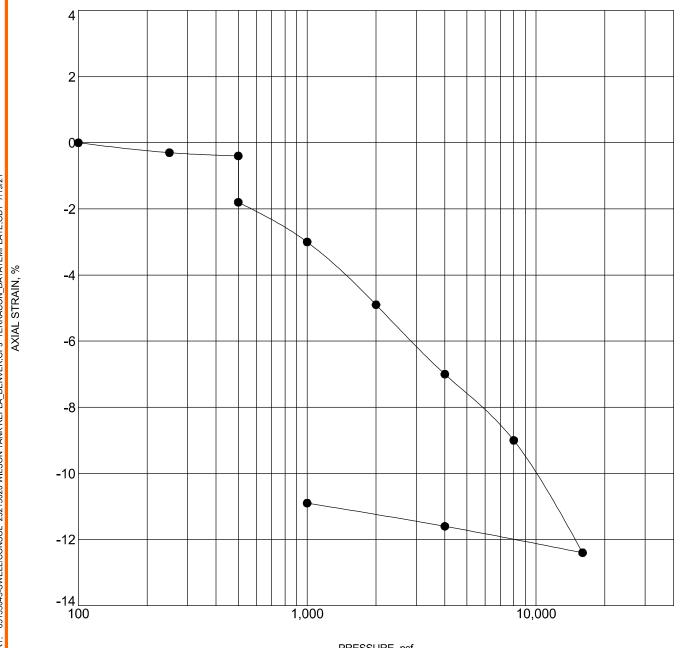
Denver, Colorado

### **GRAIN SIZE DISTRIBUTION**

**ASTM D422 / ASTM C136** 



# SWELL CONSOLIDATION TEST ASTM D4546



PRESSURE, psi	

Spe	cimen Ide	entification	Classification	$\gamma_d$ , pcf	WC, %
•	B-103	9 - 10 ft	SILTY SAND(SM)	119	2

NOTES: Sample inundated with water at 500 pounds per square foot (psf).

PROJECT: Wilson Tank Replacement

SITE: 6570 Alabaster Way Colorado Springs, Colorado

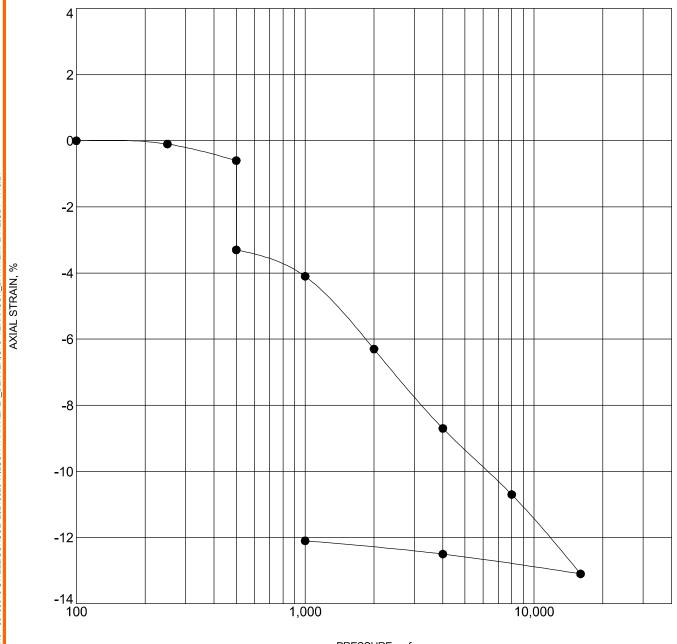


PROJECT NUMBER: 23215020

CLIENT: Kimley-Horn and Associates

Inc Denver, Colorado

# SWELL CONSOLIDATION TEST ASTM D4546



PRESSUR	E, pst	•
---------	--------	---

Specimen Identification	Classification	$\gamma_d$ , pcf	WC, %
● B-103 19 - 20 ft	SILTY SAND(SM)	112	2

NOTES: Sample inundated with water at 500 pounds per square foot (psf).

PROJECT: Wilson Tank Replacement

SITE: 6570 Alabaster Way Colorado Springs, Colorado

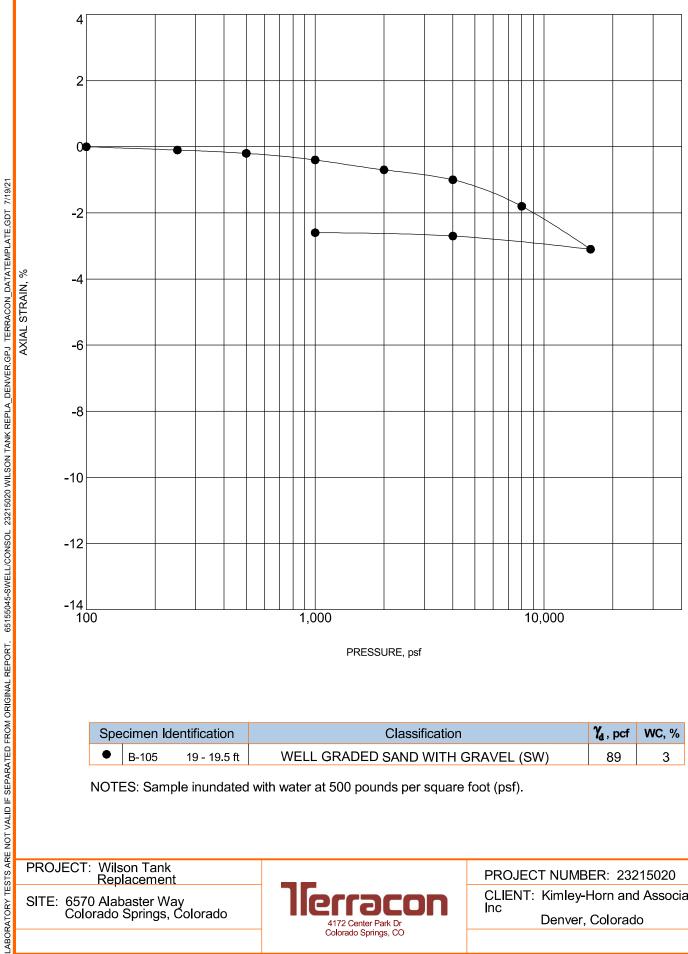


PROJECT NUMBER: 23215020

CLIENT: Kimley-Horn and Associates

Inc Denver, Colorado

# SWELL CONSOLIDATION TEST ASTM D4546



Specimen Identification			Classification	$\gamma_d$ , pcf	WC, %
•	B-105	19 - 19.5 ft	WELL GRADED SAND WITH GRAVEL (SW)	89	3

NOTES: Sample inundated with water at 500 pounds per square foot (psf).

PROJECT: Wilson Tank Replacement

SITE: 6570 Alabaster Way Colorado Springs, Colorado



PROJECT NUMBER: 23215020

CLIENT: Kimley-Horn and Associates

Inc

Denver, Colorado



## **Analytical Results**

TASK NO: 200629032

Report To: Rob Hernandez

Company: Terracon, Inc. - Colo Springs

4172 Center Park Drive Colo. Springs CO 80916 Bill To: Rob Hernandez

Company: Terracon, Inc. - Accounts Payable

18001 W. 106th St

Suite 300

Olathe KS 66061

**Task No.:** 200629032

**Client PO:** 

Client Project: CSU Wilson Tank 23205050

**Date Received:** 6/29/20 **Date Reported:** 7/6/20

Matrix: Soil - Geotech

Customer Sample ID B-1 @ 1

Lab Number: 200629032-01

Test	Result	Method
Chloride - Water Soluble	0.0017 %	AASHTO T291-91/ ASTM D4327
рН	7.8 units	AASHTO T289-91
Resistivity	7955 ohm.cm	AASHTO T288-91
Sulfate - Water Soluble	0.002 %	AASHTO T290-91/ ASTM D4327

#### Abbreviations/ References:

AASHTO - American Association of State Highway and Transportation Officials. ASTM - American Society for Testing and Materials. ASA - American Society of Agronomy. DIPRA - Ductile Iron Pipe Research Association Handbook of Ductile Iron Pipe.

DATA APPROVED FOR RELEASE BY



# **Analytical Results**

TASK NO: 210629008

Report To: Tyler Compton

Company: Terracon, Inc. - Colo Springs

4172 Center Park Drive Colo. Springs CO 80916 Bill To: Tyler Compton

Company: Terracon, Inc. - Accounts Payable

18001 W. 106th St

Suite 300

Olathe KS 66061

Task No.: 210629008

**Client PO:** 

Client Project: Wilson Tank Replacement 23215020

Date Received: 6/29/21 Date Reported: 7/6/21

Matrix: Soil - Geotech

**Customer Sample ID** B-103 @ 1-5ft **Lab Number:** 210629008-01

Test	Result	Method
Chloride - Water Soluble	0.0002 %	AASHTO T291-91/ ASTM D4327
рН	7.7 units	AASHTO T289-91
Resistivity	6743 ohm.cm	AASHTO T288-91
Sulfate - Water Soluble	< 0.001 %	AASHTO T290-91/ ASTM D4327

#### Abbreviations/ References:

AASHTO - American Association of State Highway and Transportation Officials. ASTM - American Society for Testing and Materials. ASA - American Society of Agronomy. DIPRA - Ductile Iron Pipe Research Association Handbook of Ductile Iron Pipe.

DATA APPROVED FOR RELEASE BY

### **SUPPORTING INFORMATION**

### **Contents:**

General Notes Unified Soil Classification System Global Slope Stability Results

Note: All attachments are one page unless noted above.

### **GENERAL NOTES**

**DESCRIPTION OF SYMBOLS AND ABBREVIATIONS** 

Wilson Tank Replacement Colorado Springs, Colorado

Terracon Project No. 23215020



SAMPLING	WATER LEVEL		FIELD TESTS	
Madificad	Water Initially Encountered	N	Standard Penetration Test Resistance (Blows/Ft.)	
Modified Dames & Mr. Grab Moore Ring Sample	Water Level After a Specified Period of Time	(HP)	Hand Penetrometer	
Sampler —	Water Level After a Specified Period of Time		Torvane	
Split Spoon	Cave In Encountered	(DCP)	Dynamic Cone Penetrometer	
	Water levels indicated on the soil boring logs are the levels measured in the borehole at the times indicated. Groundwater level variations will occur			
	over time. In low permeability soils, accurate determination of groundwater levels is not possible with short term water level observations.	(PID)	Photo-lonization Detector	
		(OVA)	Organic Vapor Analyzer	

#### **DESCRIPTIVE SOIL CLASSIFICATION**

Soil classification as noted on the soil boring logs is based Unified Soil Classification System. Where sufficient laboratory data exist to classify the soils consistent with ASTM D2487 "Classification of Soils for Engineering Purposes" this procedure is used. ASTM D2488 "Description and Identification of Soils (Visual-Manual Procedure)" is also used to classify the soils, particularly where insufficient laboratory data exist to classify the soils in accordance with ASTM D2487. In addition to USCS classification, coarse grained soils are classified on the basis of their in-place relative density, and fine-grained soils are classified on the basis of their consistency. See "Strength Terms" table below for details. The ASTM standards noted above are for reference to methodology in general. In some cases, variations to methods are applied as a result of local practice or professional judgment.

### **LOCATION AND ELEVATION NOTES**

Exploration point locations as shown on the Exploration Plan and as noted on the soil boring logs in the form of Latitude and Longitude are approximate. See Exploration and Testing Procedures in the report for the methods used to locate the exploration points for this project. Surface elevation data annotated with +/- indicates that no actual topographical survey was conducted to confirm the surface elevation. Instead, the surface elevation was approximately determined from topographic maps of the area.

	STRENGTH TERMS								
Density det	OF COARSE-GR/ 0% retained on No sieve.) ermined by Standation Resistance	. 200	(50%) Consistency de	or more passing	NE-GRAINED SO g the No. 200 siev oratory shear stre es or standard po ance	e.)		BEDROCK	
Descriptive Term (Density)	Standard Penetration or N-Value Blows/Ft	Ring Sampler Blows/Ft.	Descriptive Term (Consistency)	Unconfined Compressive Strength Qu, (tsf)	Standard Penetration or N-Value Blows/Ft.	Ring Sampler Blows/Ft.	Ring Sampler Blows/Ft.	Standard Penetration or N-Value Blows/Ft.	Descriptive Term (Consistency)
Very Loose	0 - 3	0-6	Very Soft	less than 0.25	0 - 1	< 3	< 30	< 20	Weathered
Loose	4 - 9	7 - 18	Soft	0.25 to 0.50	2 - 4	3 - 4	30 - 49	20 - 29	Firm
Medium Dense	10 - 29	19 - 58	Medium Stiff	0.50 to 1.00	4 - 8	5 - 9	50 - 89	30 - 49	Medium Hard
Dense	30 - 50	59 - 98	Stiff	1.00 to 2.00	8 - 15	10 - 18	90 - 119	50 - 79	Hard
Very Dense > 50 ≥ 99		Very Stiff 2.00 to 4.00 15 - 30 19 - 42			> 119	>79	Very Hard		
			Hard	> 4.00	> 30	> 42			

### **RELEVANCE OF SOIL BORING LOG**

The soil boring logs contained within this document are intended for application to the project as described in this document. Use of these soil boring logs for any other purpose may not be appropriate.



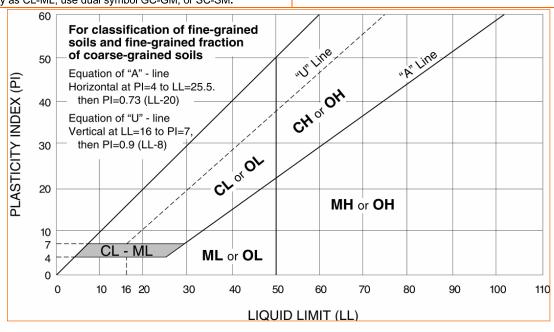
	Soil Classification					
Criteria for Assigni	ing Group Symbols	and Group Names	Using Laboratory Te	ests 🗛	Group Symbol	Group Name <sup>B</sup>
		Clean Gravels:	Cu ≥ 4 and 1 ≤ Cc ≤ 3 <sup>E</sup>		GW	Well-graded gravel <sup>F</sup>
	<b>Gravels:</b> More than 50% of	Less than 5% fines <sup>C</sup>	Cu < 4 and/or [Cc<1 or Cc	>3.0] <sup>E</sup>	GP	Poorly graded gravel <sup>F</sup>
	coarse fraction retained on No. 4 sieve	Gravels with Fines:	Fines classify as ML or MI	1	GM	Silty gravel <b>F, G, H</b>
Coarse-Grained Soils: More than 50% retained	retained on No. 4 sieve	More than 12% fines <sup>c</sup>	Fines classify as CL or CH		GC	Clayey gravel <b>F, G, H</b>
on No. 200 sieve		Clean Sands:	Cu ≥ 6 and 1 ≤ Cc ≤ 3 <sup>E</sup>		SW	Well-graded sand I
	Sands: 50% or more of coarse	Less than 5% fines D	Cu < 6 and/or [Cc<1 or Cc>3.0] E		SP	Poorly graded sand
	fraction passes No. 4	Sands with Fines:	Fines classify as ML or MI	1	SM	Silty sand <sup>G, H, I</sup>
	sieve	More than 12% fines D	Fines classify as CL or CH		sc	Clayey sand <sup>G, H, I</sup>
		Ingraphica	PI > 7 and plots on or above "A"		CL	Lean clay <sup>K, L, M</sup>
	Silts and Clays:	Inorganic:	PI < 4 or plots below "A" line J		ML	Silt K, L, M
	Liquid limit less than 50	Organic:	Liquid limit - oven dried	< 0.75	OL	Organic clay <sup>K, L, M, N</sup>
Fine-Grained Soils: 50% or more passes the		Organic.	Liquid limit - not dried	< 0.75	OL	Organic silt K, L, M, O
No. 200 sieve		Inorganic:	PI plots on or above "A" lir	ne	CH	Fat clay <sup>K, L, M</sup>
	Silts and Clays:	morganic.	PI plots below "A" line		MH	Elastic Silt K, L, M
	Liquid limit 50 or more	Organic:	Liquid limit - oven dried	< 0.75	ОН	Organic clay K, L, M, P
		Organio.	Liquid limit - not dried	\ 0.10	011	Organic silt <sup>K,</sup> L, M, Q
Highly organic soils:	Primarily	organic matter, dark in co	olor, and organic odor		PT	Peat

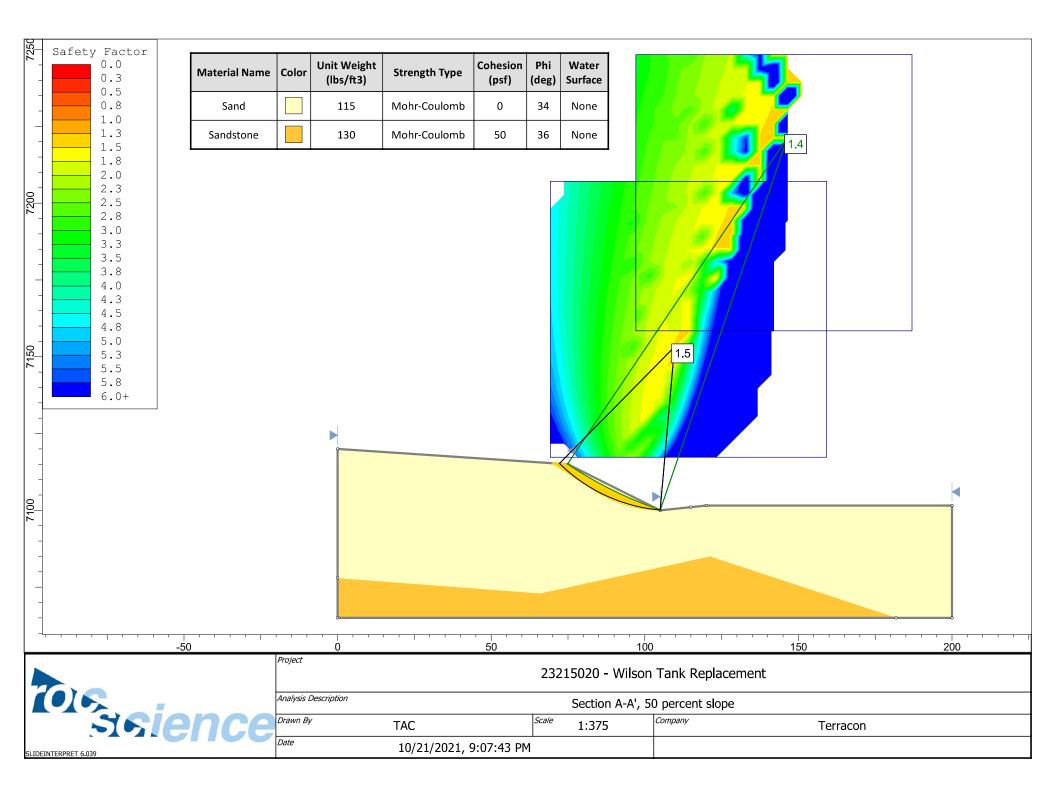
- A Based on the material passing the 3-inch (75-mm) sieve.
- <sup>B</sup> If field sample contained cobbles or boulders, or both, add "with cobbles or boulders, or both" to group name.
- Gravels with 5 to 12% fines require dual symbols: GW-GM well-graded gravel with silt, GW-GC well-graded gravel with clay, GP-GM poorly graded gravel with silt, GP-GC poorly graded gravel with clay.
- P Sands with 5 to 12% fines require dual symbols: SW-SM well-graded sand with silt, SW-SC well-graded sand with clay, SP-SM poorly graded sand with silt, SP-SC poorly graded sand with clay.

E Cu = 
$$D_{60}/D_{10}$$
 Cc =  $\frac{(D_{30})^2}{D_{10} \times D_{60}}$ 

- F If soil contains ≥ 15% sand, add "with sand" to group name.
- <sup>G</sup> If fines classify as CL-ML, use dual symbol GC-GM, or SC-SM.

- HIf fines are organic, add "with organic fines" to group name.
- If soil contains ≥ 15% gravel, add "with gravel" to group name.
- J If Atterberg limits plot in shaded area, soil is a CL-ML, silty clay.
- K If soil contains 15 to 29% plus No. 200, add "with sand" or "with gravel," whichever is predominant.
- Left soil contains ≥ 30% plus No. 200 predominantly sand, add "sandy" to group name.
- MIf soil contains ≥ 30% plus No. 200, predominantly gravel, add "gravelly" to group name.
- NPI ≥ 4 and plots on or above "A" line.
- OPI < 4 or plots below "A" line.
- PPI plots on or above "A" line.
- QPI plots below "A" line.





## COLORADO GEOLOGICAL SURVEY

1801 Moly Road Golden, Colorado 80401 303.384.2655



August 31, 2021

Karen Berry State Geologist

William Gray Planning and Community Development 30 S. Nevada Avenue, Suite 105 P.O. Box 1575, MC 155 Colorado Springs, CO 80901

**Location:** N½ SW¼ NW¼ Sec. 15 T13S, R67W of the 6<sup>th</sup> PM 38.9221°, -104.8849°

Subject: CSU Wilson Tank Site Development Plan and Final Plat, AR DP 21-00526 and AR FP 21-00527, Colorado Springs, El Paso County, CO, CGS Unique No. EP-22-0013

Dear William,

The Colorado Geological Survey (CGS) has reviewed the CSU Wilson Tank site development plan and final plat referral. We understand the applicant proposes a new water storage tank and associated site improvements at 6570 Alabaster Way. With this referral, CGS received a request for review (Emails dated August 19, 2021), Application (Kimley Horn and Associates, Inc., July 29, 2021), Development Plan (Kimley Horn, undated), Drainage Report (Kimley Horn, July 30, 2021), and Preliminary Geologic Hazards Study (Terracon Consultants, Inc., July 27, 2021). Terracon references a Geotechnical Engineering Report in their Geologic Hazards study; however, this study was not provided in the referral documents.

The site is not within any known landslides or mapped Colorado Springs landslide-susceptible area (White and Wait, 2003). CGS agrees with Terracon's assessment (page i) that the potential geologic hazards at the site that may impact the proposed development include the potential to encounter localized man-made slope instability and steeply dipping bedrock within foundation bearing elevations. Kimley Horn's development plan and available LiDAR show slopes around 50 percent descending toward the proposed tank. Terracon indicates on page 5, "Apparent signs of instability of the existing slopes in the form of scarps, surficial cracking, and/or surficial instability was not observed."

Terracon's assessment of the geologic hazards are valid; CGS offers the following comments/concerns and recommendations:

<u>Site-Specific Geology</u>: Terracon references the Pikeview 7.5 Quadrangle Geologic Map (Thornson, J.P., Carroll, C.J., and Morgan, M.L., 2001) on page 3 of the report. However, the Cascade 7.5 Quadrangle Geologic Map (Morgan et al., 2004), which encompasses the project area, is presented in the site attachments. The Cascade Quadrangle should also be referenced in the report.

<u>Faulting</u>: Terracon *does not* address the Rampart Range Fault, which is less than ½ mile from the site, nor the series of faults that may traverse the project area (Morgan et al., 2004, Geologic Map of the Cascade Quadrangle, El Paso County, Colorado, CGS). CGS recommends Terracon discuss the hazards associated with the structural features (faults) shown on the Cascade Quadrangle that traverse within and near the site in the report. CGS also recommends that appropriate seismic factors be incorporated in the design of the proposed tank structure.

Slope Stability Analysis: As noted on page 5 of Terracon's report, "The existing and proposed relatively steep slopes along the west and south sides of the proposed tank create a risk for localized man-made unstable slopes at this location." CGS agrees with Terracon's recommendation that "a slope stability analysis be performed to confirm the long term stability of the slopes." The slope stability analysis <u>must</u> be based on soil/bedrock geometry along the length of the slope section, shear strength values measured from site-specific samples and laboratory testing, and groundwater levels that may be anticipated in the area (perched conditions). Also, seismic factors should be included in the analysis that considers the Rampart Range Fault zone.

<u>Dipping Bedrock</u>: The site is located within the Hillside Overlay and is mapped about 150 feet west of an area mapped as susceptible to differential heave in expansive, steeply dipping bedrock (>30°). Terracon encountered bedrock at depths ranging from 3½ to 37 feet below the existing grade. CGS agrees with Terracon's assessment that "Although not observed in the bedrock samples obtained from our borings, it is our opinion that dipping bedrock is likely present at this site." We also agree with Terracon's recommendation "The proposed tank should be constructed on shallow foundations supported on a minimum 10-foot thick zone of structural fill, such that a minimum 10-foot separation exists between the lowest foundation element and the top of bedrock." CGS recommends that Terracon provide material properties (gradation specifications, use of on-site vs. import materials, etc.), earthwork recommendations for the structural fill material, and potential movement estimates (total and differential) if not provided in the Geotechnical Engineering Report. In addition, the project team and contractor should anticipate difficult excavation conditions within the on-site bedrock.

<u>Geo-Hazard Disclosure Statement</u>: Per the City ordinance, the statement (as presented on sheet 1 of the development plan) must list the geologic hazards identified at this site. We recommend that the City require the disclosure statement to follow the ordinance by listing the identified geologic hazards at the site.

In summary, CGS has no objection to approval of the development plan and final plat provided Terracon's recommendations are adhered to, and CGS's comments and suggestions presented in this letter are addressed.

Thank you for the opportunity to review and comment on this project. If you have questions or require further review, please call me at 303-384-2632 or email acrandall@mines.edu.

Sincerely,

any Candal

Amy Crandall, P.E. Engineering Geologist

## COLORADO GEOLOGICAL SURVEY

1801 Moly Road Golden, Colorado 80401 303.384.2655



January 14, 2022

Karen Berry State Geologist

William Gray Planning and Community Development 30 S. Nevada Avenue, Suite 105 P.O. Box 1575, MC 155 Colorado Springs, CO 80901

**Location:** N½ SW¼ NW¼ Sec. 15 T13S, R67W of the 6<sup>th</sup> PM 38.9221°, -104.8849°

Subject: CSU Wilson Tank Site Development Plan and Final Plat, AR DP 21-00526 and AR FP 21-00527, Colorado Springs, El Paso County, CO, CGS Unique No. EP-22-0013

Dear William,

The Colorado Geological Survey (CGS) has reviewed the CSU Wilson Tank site development plan and final plat resubmittal. With this resubmittal, CGS received a request for review (Email dated December 29, 2021), Comment Response Letter (Kimley Horn and Associates, Inc., December 13, 2021), Development Plan (Kimley Horn, undated), Drainage Report (Kimley Horn, July 30, 2021), Geologic Hazards Study (Terracon Consultants, Inc. (Terracon), Revised November 18, 2021), and Geotechnical Engineering Report (Terracon, Revised November 18, 2021).

Terracon's revised geologic hazards report and geotechnical engineering report adequately address our previous comments and concerns. For example, Terracon's slope stability analysis presented in the geotechnical engineering report for the proposed slopes and the discussion of long-term slope stability address our concerns regarding the steep slopes along the west and south sides of the proposed tank. Terracon's recommendations for surficial slope stability (page 15) should be strictly adhered to. Specifically, "Irrigated landscaping should not be used on or near the crest of slopes" and "Slopes should be re-vegetated as soon as possible after grading and protected from erosion until vegetation is established."

Provided Terrcon's recommendations are adhered to, CGS has no objection to approval of the development plan and final plat.

<u>Geo-Hazard Disclosure Statement</u>: Per the City ordinance, the statement (as presented on sheet 1 of the development plan) must list the geologic hazards identified at this site and reference Terracon's most up-to-date geologic hazard report (November 18, 2021). We recommend that the City require the disclosure statement to follow the ordinance by listing the identified geologic hazards at the site.

Thank you for the opportunity to review and comment on this project. If you have questions or require further review, please call me at 303-384-2632 or email acrandall@mines.edu.

Sincerely,

Amy Crandall, P.E. Engineering Geologist

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